**Universal Published Paper Review**

Introduction

The Quinn Fluid Flow Model (QFFM) is a totally new and novel theory of fluid dynamics in closed conduits. The underlying intellectual property is owned by The Wrangler Group LLC (TWG). It has been developed from first principles and applies to fluid flow in both packed and empty conduits across the entire fluid flow regime including laminar, transitional and turbulent. The model has been validated by applying it to classic studies in both categories of flow embodiments and, in each case, to studies in all fluid flow regimes.

The QFFM can be expressed in two formats. The first format is a dimensional manifestation in which the measured differential pressure across the ends of a conduit is compared to the measured resultant flow rate of the fluid according to the relationships dictated by the model among the many independent and dependent variables pertaining to the physical fluid flow embodiment and pertaining to the fluid itself. The second format is a dimensionless manifestation, which we call Quinn’s Law, where all the individual respective contributions to the pressure drop/fluid flow relationship have been normalized between the model’s two entities, which we call the “Quinn reduced pressure” and the “fluid current” and which we denote with the symbols PQ and Qc, respectively.

Any given combination of the underlying variables prescribed by the QFFM will have a unique pressure drop at any given flow rate. Accordingly, the QFFM is capable of distinguishing between *valid* and *invalid* data. In particular, the QFFM can identify a mismatch between a practitioner’s statement of the values he/she claims to have measured or calculated for the QFFM variables and the practitioner’s measured flow rate and pressure drop. We consider any mismatch to be an *invalid* empirical result. It follows that for every *invalid* empirical result there is but one *valid* corrected result.

Before one can apply Quinn’s Law to any given empirical result that result has to be validated using the dimensional manifestation of the QFFM. This, in turn, is because one cannot normalize properly for all the individual respective contributions unless all the variables are correctly identified and their values are commensurate with the measured pressure drops and fluid flow rates. In general, we can state that since most of the underlying variables pertaining to a fluid flow embodiment are relatively easy to measure, the correction usually pertains to the more difficult-to-measure variables. In the case of a packed conduit, the problematical measurements include particle sphericity, average particle diameter and conduit external porosity, In the case of an empty conduit, the weak link in terms of measurability is the conduit’s inner wall roughness.

QFFM is a unique and powerful new tool in the arsenal of the fluid flow practitioner. In particular, when experiments are conducted in the transitional and/or turbulent regimes, the conventional methodology does not provide any reliable way to verify the accuracy of the results across a broad spectrum of Reynolds numbers. Thus, it is in these regions of the fluid flow regime that the QFFM will be shown to be most useful. In fact, it is a direct consequence from the statements contained herein that one needs only to measure pressure drop and fluid flow rate to evaluate the quality of one’s experimental technique. This new development in fluid dynamics means that those of us who have spent our entire lives doing fluid flow measurements can now enjoy the same benefits as our counterparts within the field of electricity and magnetism.

Paper Summary

We review here a published article in ***Applied Physics and Engineering 17 (2), 89-100, 2016*,** entitled **Pressure drop in a packed bed with sintered ore particles as applied to sinter coolers with a novel vertically arranged design for waste heat recovery*,*** by **Tian et al**. Because the abstract is missing in the particular copy of the paper that we are working from, we include the section 4.5 in the paper entitled **Pressure drop correlation.**

**4.5 Pressure drop correlation**

For the unsorted and sieved SOPs, a total number of 370 experimental data points for the modified friction factor were collected for the modified Re number range from 500 to 12,000, as presented elsewhere. This range of modified Re number covers all the flow regimes from laminar to turbulent. In general, the data points collapse on a single curve regardless of the size range. Using the modified Ergun equation, Eq. (14), as the model equation, a correlation for the modified friction factor was obtained by curve fitting, which reads as follows; fm = 213 +8.8Rem0.87, with R2 =0.989. Almost all the data points lie in the ± 10% range of this correlation. As shown elsewhere, it is interesting that the present correlation is in agreement with that proposed by Allen et al., (2013) for the pressure drop through rock beds, which is given by; fm = 200 +8Rem0.88,

**Data Analysis**

TWG has performed an extensive evaluation of the above referenced published article utilizing the QFFM. We commence our evaluation of the paper with an in-depth analysis of the reported data.

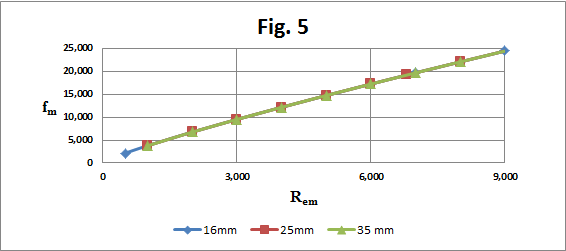
**Fig. A**

In our Fig. A herein, we use the modified Ergun equation with constants of 213 and 8.8 for the viscous and kinetic constants, respectively, to create a replica of Fig. 9 in the paper using the raw underlying fluid flow conduit parameters reported in the paper for the glass beads and the SOPs. This corroborates the fact that we have correctly captured all the underlying parameters in the Ergun equation pertaining to the experiments with the SOPs, since our Fig1, is identical to Fig. 9 in the paper.

**Fig. B**

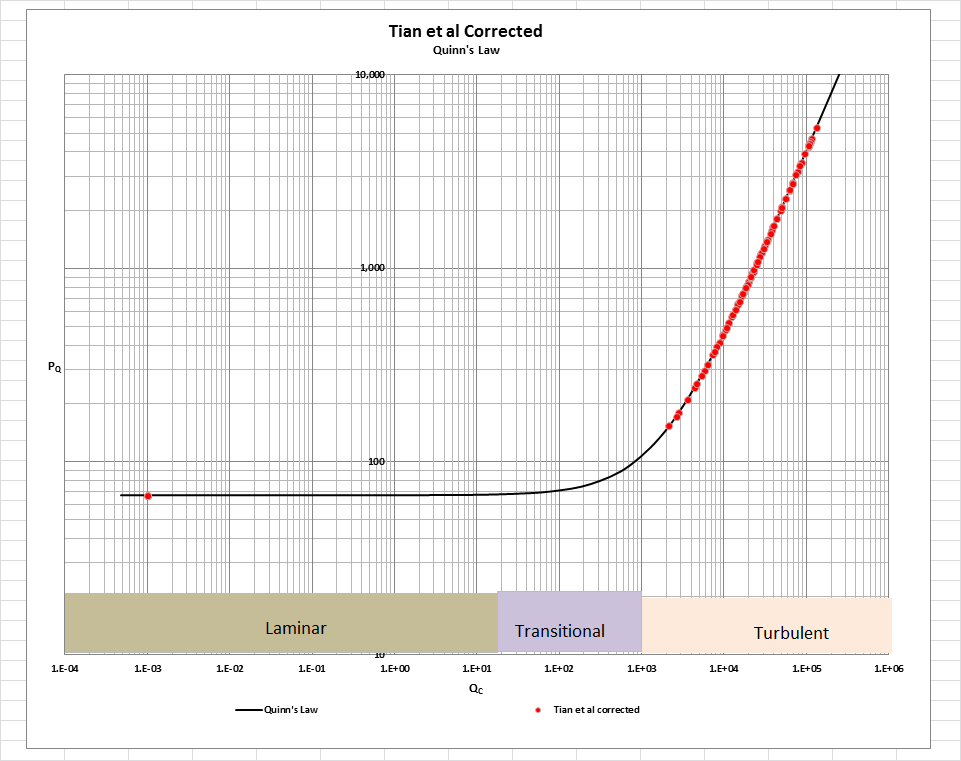
In our Fig.B herein we plot the same data as in our Fig.A for the SOPs except we use the dimensional parameters specified as in Fig. 7 in the paper, superficial velocity on the x axis and reduced pressure on the y axis. We can immediately see that our Fig.B does not correlate to Fig. 7 in the paper. Our calculated values for the reduced pressure are significantly greater than those of the authors.

**Fig. C**



In our Fig. C , we show a plot of the same data as in our Fig. A for the spherical glass spheres except that the axes of the plot are the same as those of Fig. 5 in the paper. It is clear that our plots in figures B and C do not coincide with the data displayed in figures 6 and 7 in the author’s paper. This demonstrates that there is some discrepancy between the authors measured data and their calculations of that data in the form of the modified Ergun friction factor.

**Fig. D**



In Fig. D herein, we have provided our validation of the paper’s corrected data by a comparison of the data to Quinn’s Law. This normalized relationship is presented herein in the form of a plot of PQ versus QC, whichis the frame of reference of Quinn’s Law. This frame of reference is a transformation derived from the dimensional fluid flow relationship embedded in the QFFM. The relationship between these two unique reduced Quinn parameters is *linear*. However, we chose to present it as a *log-log plot* herein to provide emphasis at both extremes of the fluid flow regime. This plot is based upon both our own experimental data and *independent accepted classical reference data* which cover flow in both packed and empty conduits, over the entire fluid flow regime. (Note that the three distinct flow regimes of laminar, transitional and turbulent are clearly marked in the log-log plot.) As can be seen, the data reported in this paper, as corrected and as displayed in the form of a plot of PQ versus QC , lines up perfectly with Quinn’s Law

[Note: we do not herein provide the back-up for the validation of the plot of Quinn’s Law depicted in our Fig. B. For a description of the sources, both personal to TWG and from independent accepted classical references, on the basis of which the Quinn’s Law plot was validated, see the general introduction to this Universal Published Paper Review tab.

**Conclusion.**

We conclude that the results in this paper suffer from deficiencies in the experimental protocols used in the experiments. As a result, there is a mismatch between the measured variables and the measured pressure drop. This mismatch is only *apparent and quantifiable* in the context of the QFFM and, therefore, can only be corrected using this model. Accordingly, since the authors did not have access to Quinn’s Law when they wrote the paper, they *could not have* corrected the data before attempting to rationalize it by applying the model of Ergun. This inherent tendency to *modify* existing equations to correlate *unsubstantiated* empirical measurements has long since contributed to the confusion that exists in this field of study and has had a tendency to create the *false illusion* that these so-called conventional equations are of some *value* when, in reality, they are nothing more than *invalid* relationships.

Moreover, even if the authors applied the classical unmodified equations of Ergun or Forchheimer, for instance, or their own newly-minted modified Ergun equation, they could not have generated *the* match inherent in the Laws of Nature between the calculated pressure drops of their chosen equation and their own measured pressure drops – unless, of course, they had serendipitously, or otherwise, identified the same *unique* equation as that embedded in the QFFM.

Finally, although a detailed evaluation of the experiments reported in the paper under review, including an identification and quantification of the specific variables in each fluid flow embodiment which we claim the QFFM prescribes need to be corrected, is clearly within the capability of TWG, concerns about maintaining the confidentiality of the QFFM and Quinn’s Law – which, at this time, are still proprietary - dictate that such a development is premature.