**Universal Published Paper Review**

Introduction

The Quinn Fluid Flow Model (QFFM) is a totally new and novel theory of fluid dynamics in closed conduits. The underlying intellectual property is owned by The Wrangler Group LLC (TWG). It has been developed from first principles and applies to fluid flow in both packed and empty conduits across the entire fluid flow regime including laminar, transitional and turbulent. The model has been validated by applying it to classic studies in both categories of flow embodiments and, in each case, to studies in all fluid flow regimes.

The QFFM can be expressed in two formats. The first format is a dimensional manifestation in which the measured differential pressure across the ends of a conduit is compared to the measured resultant flow rate of the fluid according to the relationships dictated by the model among the many independent and dependent variables pertaining to the physical fluid flow embodiment and pertaining to the fluid itself. The second format is a dimensionless manifestation, which we call Quinn’s Law, where all the individual respective contributions to the pressure drop/fluid flow relationship have been normalized between the model’s two entities, which we call the “Quinn reduced pressure” and the “fluid current” and which we denote with the symbols PQ and Qc, respectively.

Any given combination of the underlying variables prescribed by the QFFM will have a unique pressure drop at any given flow rate. Accordingly, the QFFM is capable of distinguishing between *valid* and *invalid* data. In particular, the QFFM can identify a mismatch between a practitioner’s statement of the values he/she claims to have measured or calculated for the QFFM variables and the practitioner’s measured flow rate and pressure drop. We consider any mismatch to be an *invalid* empirical result. It follows that for every *invalid* empirical result there is but one *valid* corrected result.

Before one can apply Quinn’s Law to any given empirical result that result has to be validated using the dimensional manifestation of the QFFM. This, in turn, is because one cannot normalize properly for all the individual respective contributions unless all the variables are correctly identified and their values are commensurate with the measured pressure drops and fluid flow rates. In general, we can state that since most of the underlying variables pertaining to a fluid flow embodiment are relatively easy to measure, the correction usually pertains to the more difficult-to-measure variables. In the case of a packed conduit, the problematical measurements include particle sphericity, average particle diameter and conduit external porosity, In the case of an empty conduit, the weak link in terms of measurability is the conduit’s inner wall roughness.

QFFM is a unique and powerful new tool in the arsenal of the fluid flow practitioner. In particular, when experiments are conducted in the transitional and/or turbulent regimes, the conventional methodology does not provide any reliable way to verify the accuracy of the results across a broad spectrum of Reynolds numbers. Thus, it is in these regions of the fluid flow regime that the QFFM will be shown to be most useful. In fact, it is a direct consequence from the statements contained herein that one needs only to measure pressure drop and fluid flow rate to evaluate the quality of one’s experimental technique. This new development in fluid dynamics means that those of us who have spent our entire lives doing fluid flow measurements can now enjoy the same benefits as our counterparts within the field of electricity and magnetism.

Paper Summary

We review here a published article in **Als Dissertation genehmigt von der**

**Technischen Fakultat der Universitat Erlangen-Nurnberg,** entitled **Fully Developed Turbulent Smooth and Rough Channel and Pipe Flows** *by* **Saleh**. For easy reference to the reader, we print here in its entirety the abstract in the paper.

**Paper Abstract**

In this thesis, fully developed, turbulent channel flows with smooth walls, with

one rough and one smooth wall and with two rough walls, were studied, providing

some useful and extended information about these kinds of flows. Fully developed, turbulent plane smooth channel flows were studied theoretically and experimentally. A Reynolds number range up to 1.1 x 105 was covered. The value of the von Karman constant, k, was found to be 1/e for this kind of flow, confirming the recent findings of Zanoun and Durst [2003].

Similarity conditions between channel flows with smooth surfaces, which possess

different dimensions, were investigated theoretically. Experiments were carried

out to check the theoretical findings and very good agreement was obtained.

Another objective of the present work concerned fully developed, turbulent

plane channel flows with one rough and one smooth wall. This kind of

flow shows interesting properties that have not been studied systematically, in

spite of the availability of suitable experimental and numerical means. The

maximum velocity lies off-centre, closer to the smooth wall, and its location is not

identical to that of zero shear stress of the flow. Furthermore, the mean velocity

distribution close to the rough wall can only be plotted in wall coordinates if the

wall location for zero shear stress could be defined. Methods to do this are given

utilising a two-component LDA system that was employed to measure the mean

velocity profiles and the Reynolds stress profiles for exact determination of the

corresponding position of the zero shear stress. Using the available theoretical

and experimental facilities, the effective height of the channel was determined as

well as the reference point, which is the middle of the channel, for the velocity

measurements.

Fully developed, turbulent plane channel flows with rough surfaces were

also studied in some depth. Previously, to calculate the shift between the smooth

log law lines and the rough ones, one needed information about the height of

the employed roughness. Without roughness height information, theoretical

investigations were carried out to calculate the shift between the smooth log law

line and the rough ones. The procedure was confirmed through corresponding

experimental measurements. Furthermore, a new method to measure the static

pressure in the rough regime was successfully introduced using Pitot tubes.

Finally, some of the theoretical findings were confirmed by the data of

Nikuradse, available in the literature, for smooth and the rough pipe flows.

**Data Analysis**

TWG has performed an extensive evaluation of the above referenced published article utilizing the QFFM. We commence our evaluation of the paper with an in-depth analysis of the reported data.

In our Fig. A-1 herein, we show an elaboration of Fig. 5.2 in the paper for the experimental data reported for the small smooth channel. As can be seen in the plot, the reported data needs to be corrected using the QFFM in order to align the measured pipe roughness with the measured data. It is clear from the plot that the inner wall of the channel is not hydrodynamically smooth as asserted by the author. As demonstrated by the QFFM plot the measured data deviates from that of a hydrodynamically smooth wall at a value of approximately 25,000 for the Reynolds number.

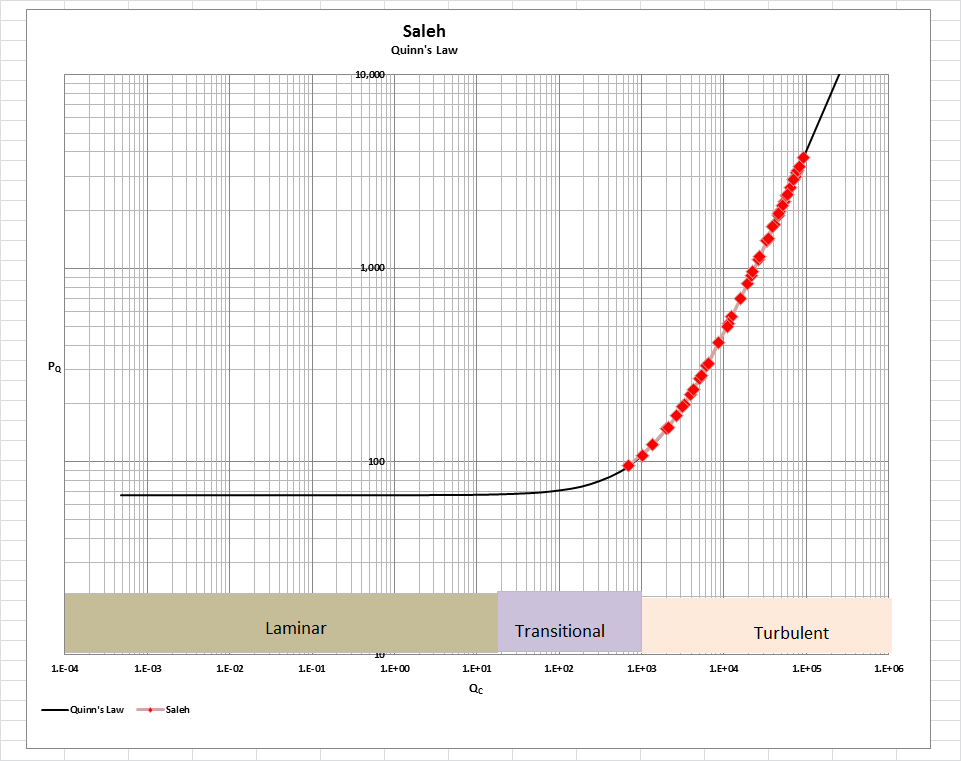
**Fig. A-1**

In our Fig. A-2 herein, we show an elaboration of Fig. 5.2 in the paper for the experimental data reported for the large smooth channel. As can be seen in the plot, the reported data needs to be corrected using the QFFM in order to align the measured pipe roughness with the measured data. It is clear from the plot that the inner wall of the channel is not hydrodynamically smooth as asserted by the author. As demonstrated by the QFFM plot the measured data deviates from that of a hydrodynamically smooth wall at a value of approximately 45,000 for the Reynolds number. This is consistent with the larger diameter pipe as compared to the small smooth channel.

**Fig. A-2**

In Fig. B herein, we have provided our validation of the papers corrected data by a comparison of the data to Quinn’s Law. This normalized relationship is presented herein in the form of a plot of PQ versus QC, whichis the frame of reference of Quinn’s Law. This frame of reference is a transformation derived from the dimensional fluid flow relationship embedded in the QFFM. The relationship between these two unique reduced Quinn parameters is *linear*. However, we chose to present it as a *log-log plot* herein to provide emphasis at both extremes of the fluid flow regime. This plot is based upon both our own experimental data and *independent accepted classical reference data* which cover flow in both packed and empty conduits, over the entire fluid flow regime. (Note that the three distinct flow regimes of laminar, transitional and turbulent are clearly marked in the log-log plot.) As can be seen, the data reported in this paper, as corrected and as displayed in the form of a plot of PQ versus QC , lines up perfectly with Quinn’s Law

**Fig. B**



[Note: we do not herein provide the back-up for the validation of the plot of Quinn’s Law depicted in our Fig. B. For a description of the sources, both personal to TWG and from independent accepted classical references, on the basis of which the Quinn’s Law plot was validated, see the general introduction to this Universal Published Paper Review tab.

**Conclusion.**

We conclude that the results in this paper suffer from deficiencies in the experimental protocols used in the experiments. As a result, there is a mismatch between the measured variables and the measured pressure drop. This mismatch is only *apparent and quantifiable* in the context of the QFFM and, therefore, can only be corrected using this model. Accordingly, since the author did not have access to Quinn’s Law when he wrote the paper, he *could not have* corrected the data before attempting to rationalize it by applying the conventional Law of the Wall. This inherent tendency to *modify* existing equations to correlate *unsubstantiated* empirical measurements has long since contributed to the confusion that exists in this field of study and has had a tendency to create the *false illusion* that these so-called conventional equations are of some *value* when, in reality, they are nothing more than *invalid* relationships.

Moreover, even if the author applied the classical Law of the Wall, for instance, or his own newly-minted modified version thereof, he could not have generated *the* match inherent in the Laws of Nature between the calculated pressure drops of his chosen equation and his own measured pressure drops – unless, of course, he had serendipitously, or otherwise, identified the same *unique* equation as that embedded in the QFFM.

Finally, although a detailed evaluation of the experiments reported in the paper under review, including an identification and quantification of the specific variables in each fluid flow embodiment which we claim the QFFM prescribes need to be corrected, is clearly within the capability of TWG, concerns about maintaining the confidentiality of the QFFM and Quinn’s Law – which, at this time, are still proprietary - dictate that such a development is premature.